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# **On the Use of Hot-Film Sensors in the Investigation of Fluid Dynamic Phenomena in the Near-Wall Region**

**Philip C. Griffin & Mark R.D. Davies**

**Stokes Research Institute**

**Department of Mechanical & Aeronautical Engineering**

**University of Limerick**

**Limerick**

**Ireland**

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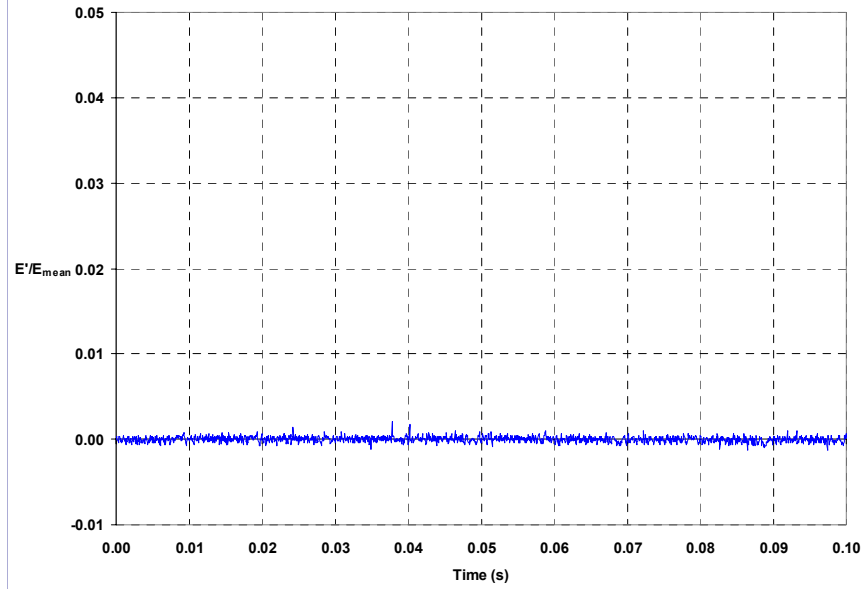
# Overview

- **Introduction and Nature of the Problem:**
- **Experimental Methods:**
  - Test Rig – Subsonic Cascade.**
  - Hot-Wire & Film Specifications.**
  - Wire-Film Correlation.**
- **Experimental Results:**
  - Correlation between a hot-wire and film operating simultaneously in a turbulent boundary layer.**
  - Wavelet analysis techniques.**
  - Hot-film surface roughness measurements.**
- **Conclusions.**

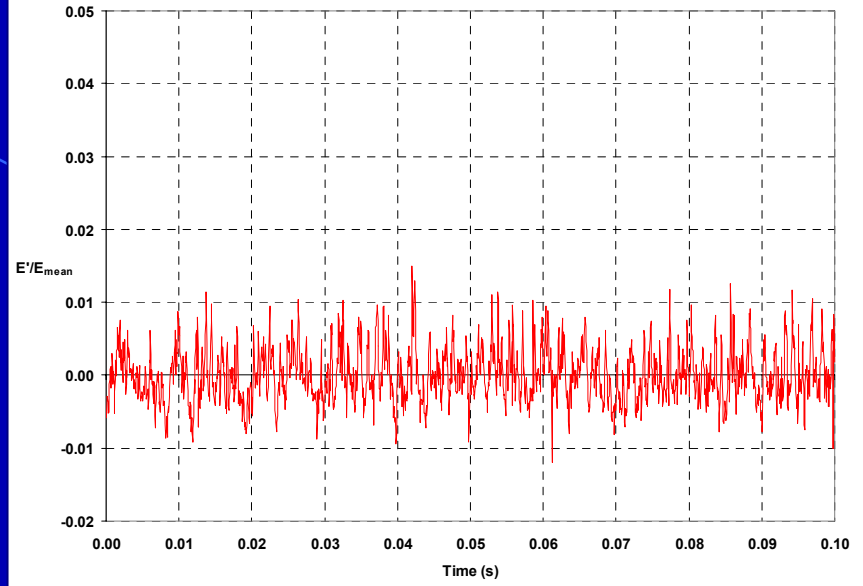
# Introduction & Nature of the Problem

- Focus is on the physics of the near-wall region.
- From a loss measurement perspective, this region constitutes most of the loss in a turbulent boundary layer due to:
  - Viscous Dissipation
  - Reynolds Stress Production
- Hot-film sensors respond to velocity fluctuations and can be used to determine the nature of the boundary layer over a surface.
- As turbulent energy is dissipated in the near-wall region by viscosity, theoretically turbulent fluctuations should approach zero at the wall.
- How can sensors that form the wall detect such fluctuations?

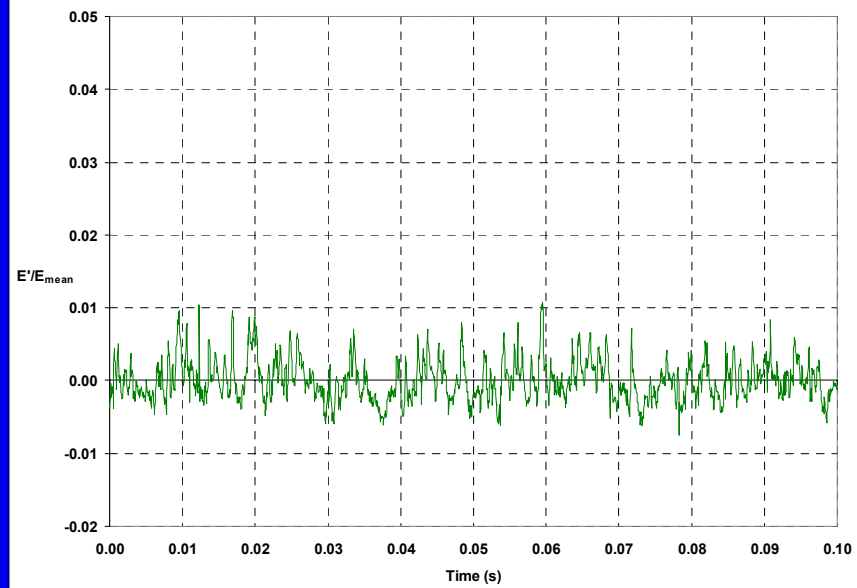
Laminar



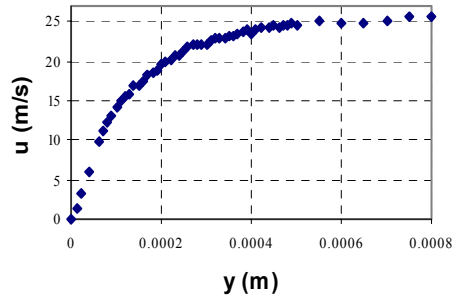
Transition



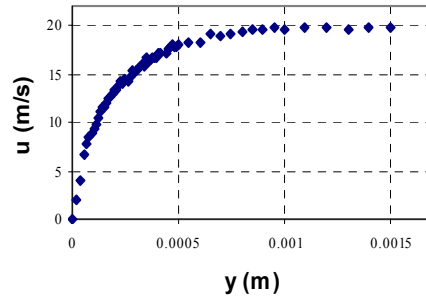
Turbulent



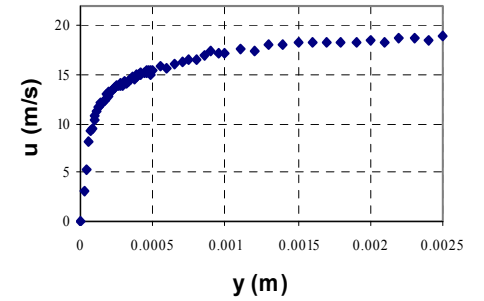
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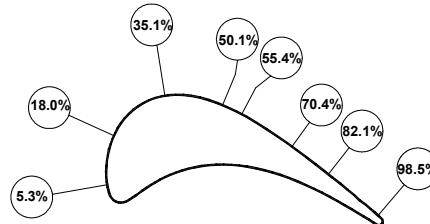
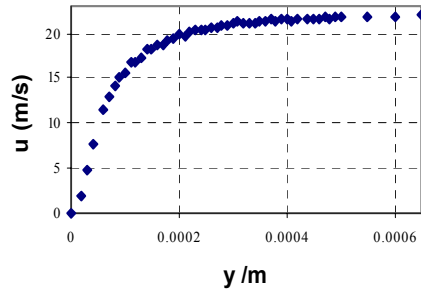
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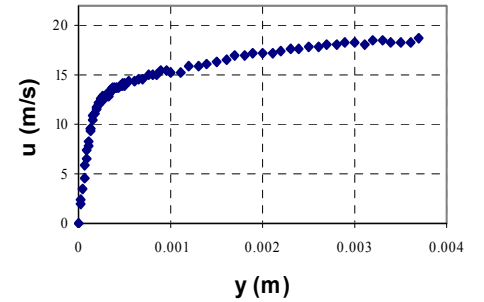
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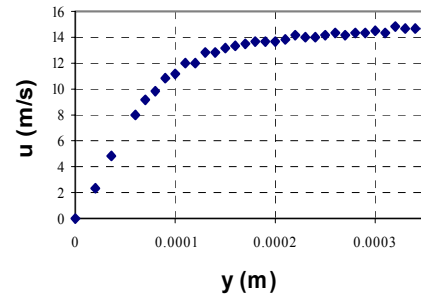
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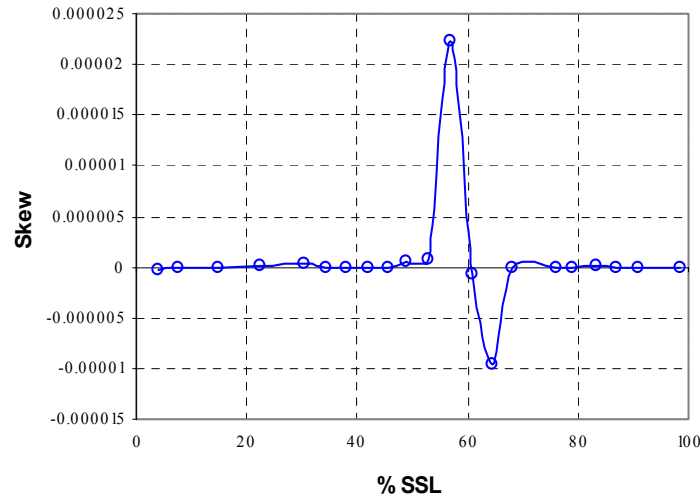
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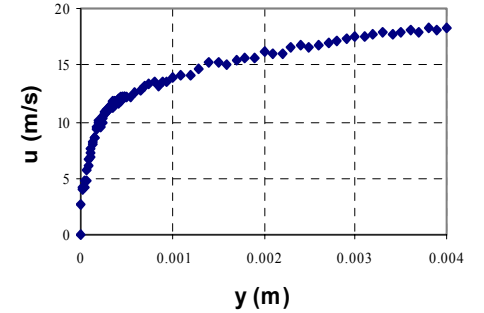
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Skew Distribution Derived From Fluctuating Hot Film Voltage Signals



95% SSL

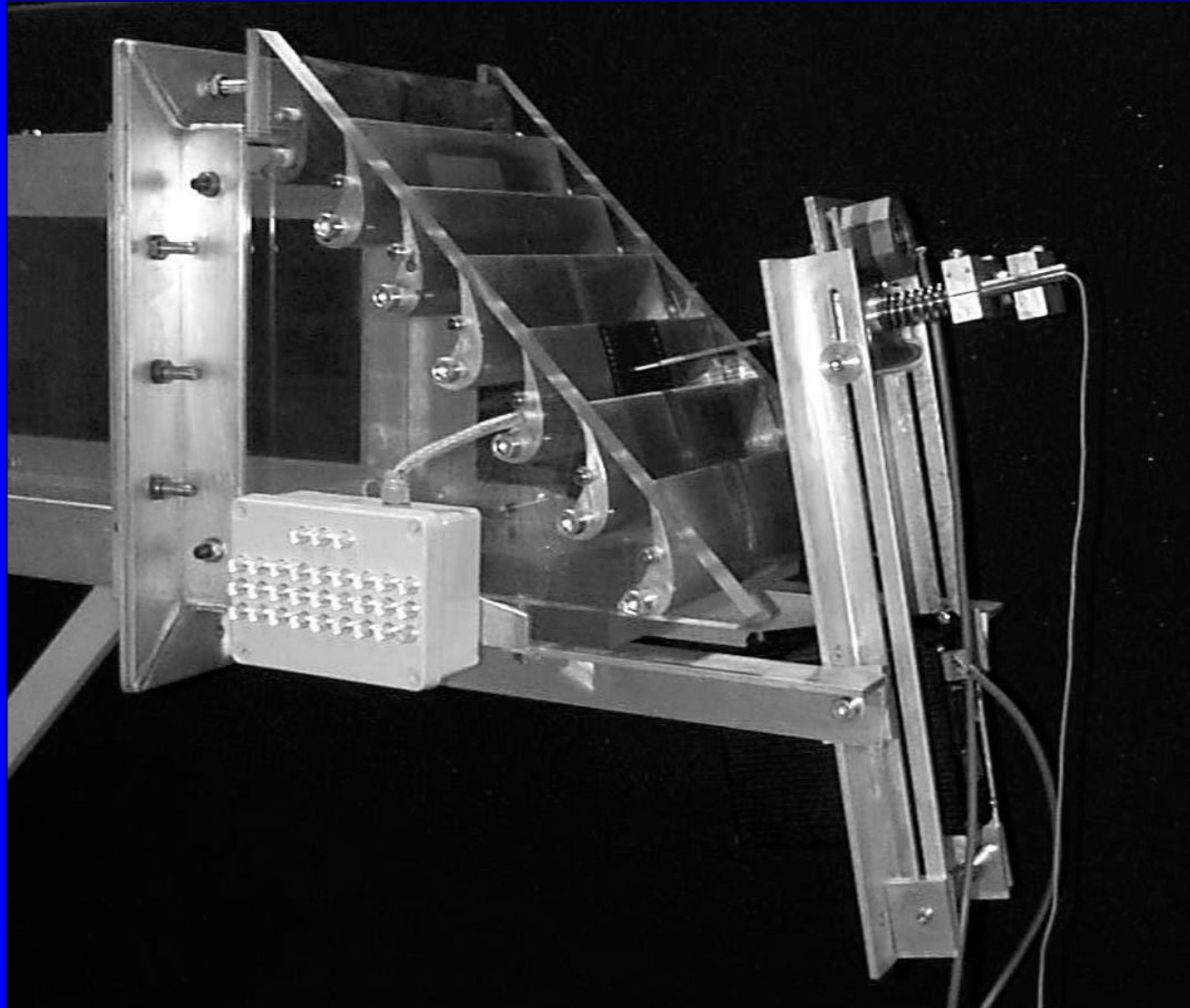


Measured Hot Wire Boundary Layer Velocity Profiles  $Re_c = 76,000$  & 5.2% Free Stream Turbulence

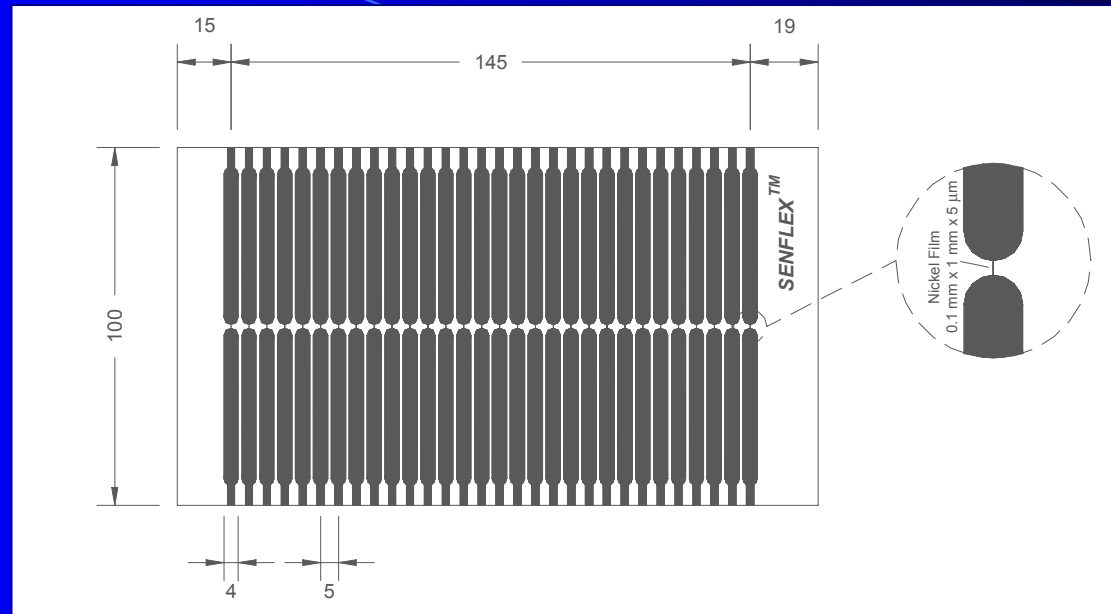
# Introduction & Nature of the Problem

- Hot-film sensors should not be sensitive to velocity due to the no-slip condition.
- Classical view - no-slip condition arises due to adsorption of gas molecules onto a solid surface.
- However no surface is perfectly smooth to an atomic level.
- Even the most finely polished surface has roughness elements (asperities) that are substantially larger than the gas molecules.
- Perhaps, the fluid is brought to rest due to the tortuous path taken around the roughness elements.
- Will look at surface finish later.

# Experimental Methods – Subsonic Cascade



# Hot-Film Array Specification



- Sensor elements are manufactured from Nickel and are electrodeposited onto a polyimide substrate.
- Sensor dimensions:  
 $1.44 \text{ mm} \times 100 \text{ } \mu\text{m} \times 0.2 \text{ } \mu\text{m}$
- Surface finish for electrodeposited materials is typically of the order of  $0.02 \text{ } \mu\text{m}$ .

# Experimental Methods - Wire-Film Correlation

- Correlation between readings from a hot-wire and hot film in the turbulent boundary layer at 76.6% SSL with  $Re = 76,000$  and 5.2% FST.
- Simultaneous operation of a hot film at  $130^{\circ}C$  and a Dantec 55P11 hot wire probe ( $250^{\circ}C$ ) while traversing from  $10 \mu m$  to 4 mm in the wall-normal direction.
- 20 kHz sampling frequency over 0.1 second duration.
- Physical Significance of the Correlation Coefficient ( $\rho_{12}$ ):

$$\rho_{12} = \frac{\overline{(U_1 - \bar{U}_1)(U_2 - \bar{U}_2)}}{\sigma_1 \sigma_2} = \frac{\overline{u_1' u_2'}}{\sqrt{\overline{u_1'^2}} \cdot \sqrt{\overline{u_2'^2}}}$$

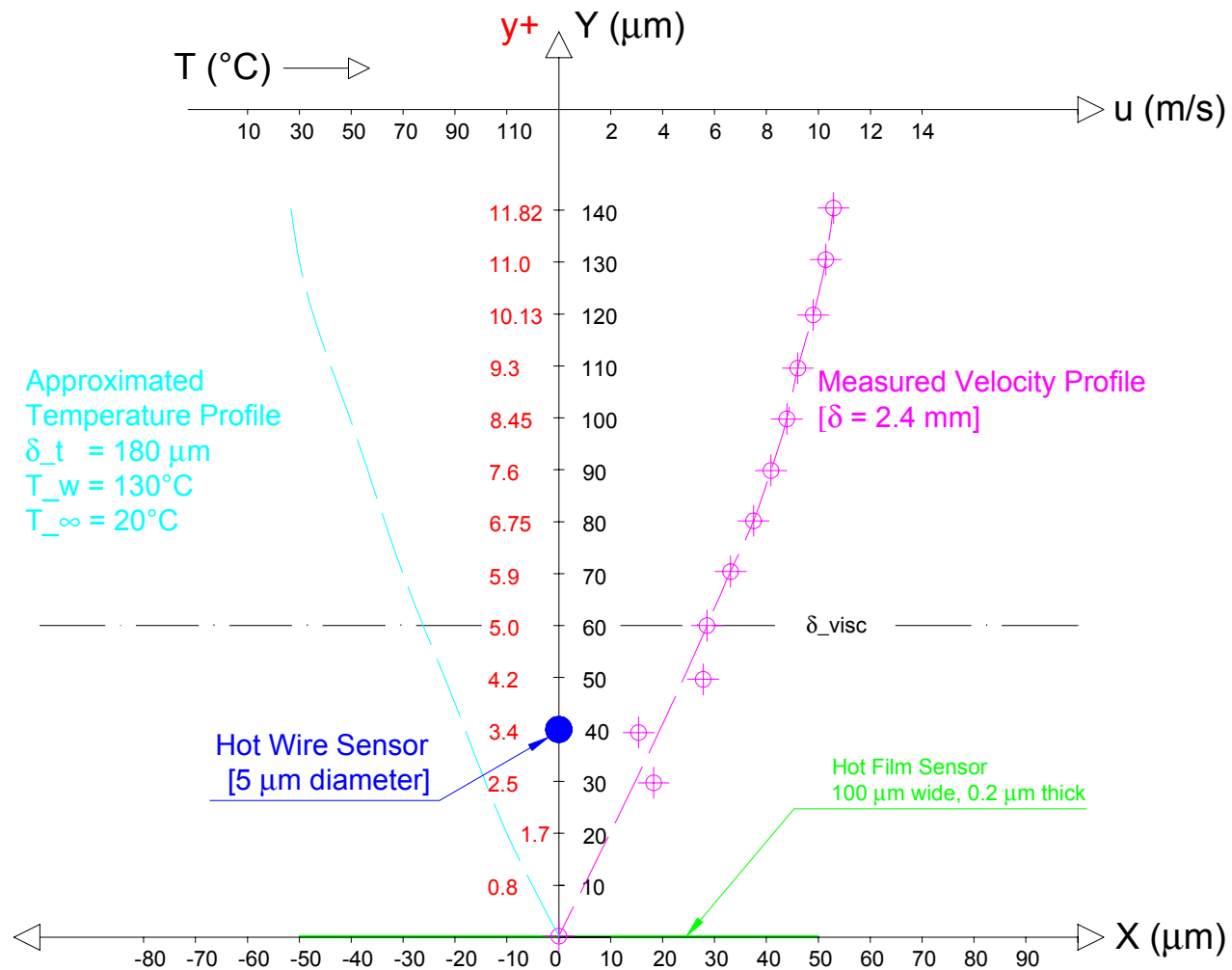
- If  $\rho_{12} = 1$ , then both wire and film are sensing the same phenomenon.
- If  $\rho_{12} = 0$ , then wire and film are not sensing the same phenomenon.

(statistically independent variables)

# Experimental Methods - Wire-Film Correlation

- Operating both a wire and film together poses problems:
  - Thermal boundary layers from both wire and film interfere with each other close to the wall.
  - Therefore inaccurate results will be obtained in this region
  - Correction of the hot-wire readings for near-wall effects made difficult.
- $\delta_t$  was estimated to be approximately 180  $\mu\text{m}$ , but the effects of the thermal boundary were only prevalent within 60  $\mu\text{m}$  of the wall.
- All data influenced by the thermal boundary layer was neglected.

# Scale of the Problem

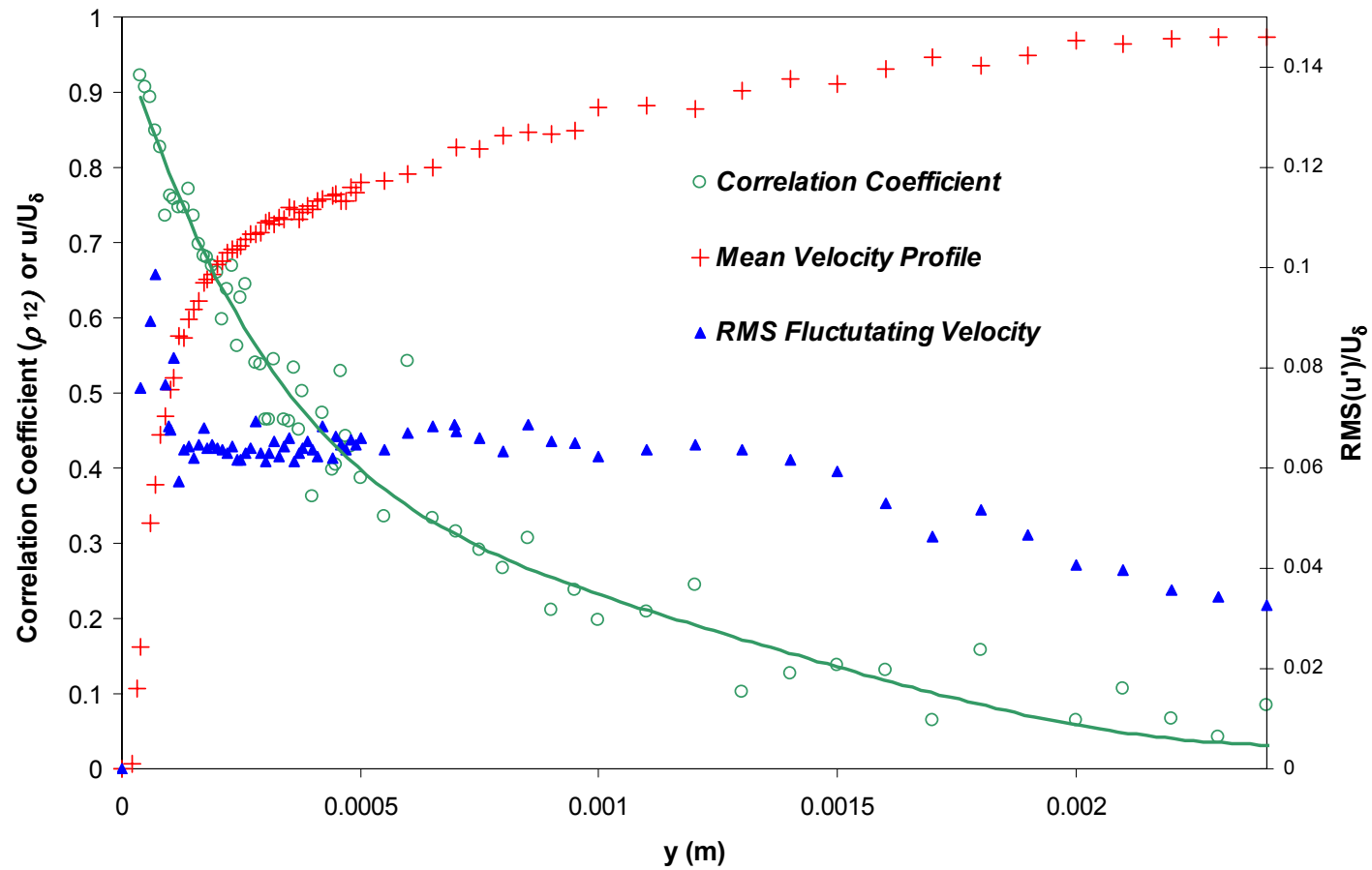


# Experimental Results - Summary

1. **Wire-film correlation distribution through the turbulent boundary layer at 76.6% SSL, and 5.2% FST.**
2. **Wavelet analysis of the simultaneously sampled wire and film data.**
3. **Measurements of the surface roughness of the hot-film sensor using Atomic Force Microscopy (AFM).**

# Wire-Film Correlation

Wire-Film Correlation across a Turbulent Boundary Layer (76.6% SSL,  $Re_c = 76,000$ , 5.2% FST &  $\delta = 2.4$  mm)



# Wavelet Analysis Methods

- Wavelet methods permit localisation of intermittent data both in frequency and time domain.
- Approach is similar to a Fourier Transform, time series is convoluted with compressed and dilated forms of a detector function known as the “Mother Wavelet”  $\psi(t)$ .
- The detector function can be any real or complex valued function that satisfies the “Admissibility Criterion” (zero mean).

$$\int_{-\infty}^{+\infty} \psi(t) dt$$

- Wavelet is compressed/dilated and time shifted, to yield a matrix corresponding to all times and frequencies in the signal.

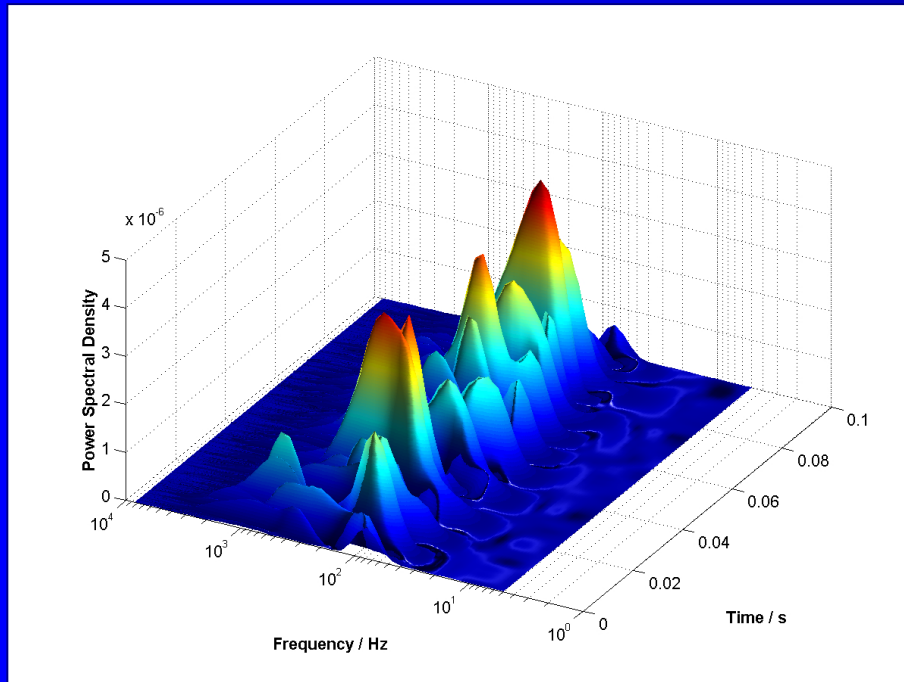
$$\Psi_{(\omega, \tau)}(t) = \frac{1}{\sqrt{\omega}} \psi\left(\frac{t - \tau}{\omega}\right)$$

# Wavelet Analysis Methods

- Convoluting with time series completes the transform, generating a 3-D time-frequency representation of the signal.
- Choice of Wavelet depends on the application.
- In this study the Marr Wavelet (second derivative of the Gaussian function) was used.
- 41 frequencies (spaced evenly on a log scale from 5-5kHz) were scanned at 2000 time increments from 0 to 0.1 seconds.
- Data was filtered to remove AC mains noise (50 Hz)
- Wavelet transforms and data filtering implemented in MATLAB™

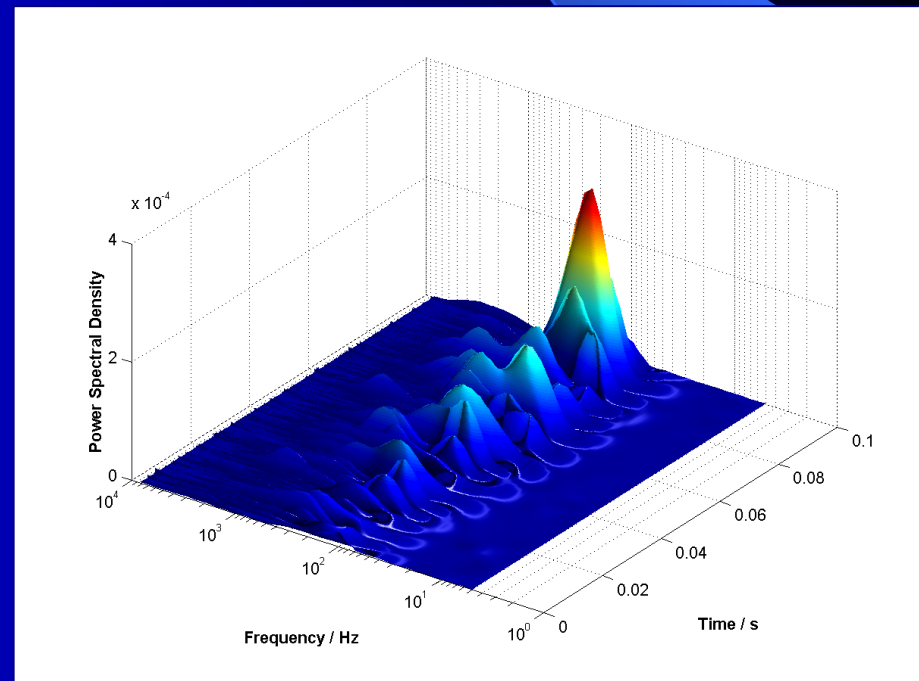
# Wavelet Analysis Methods

## Simultaneous Wire-Film Signals in a Turbulent Boundary Layer



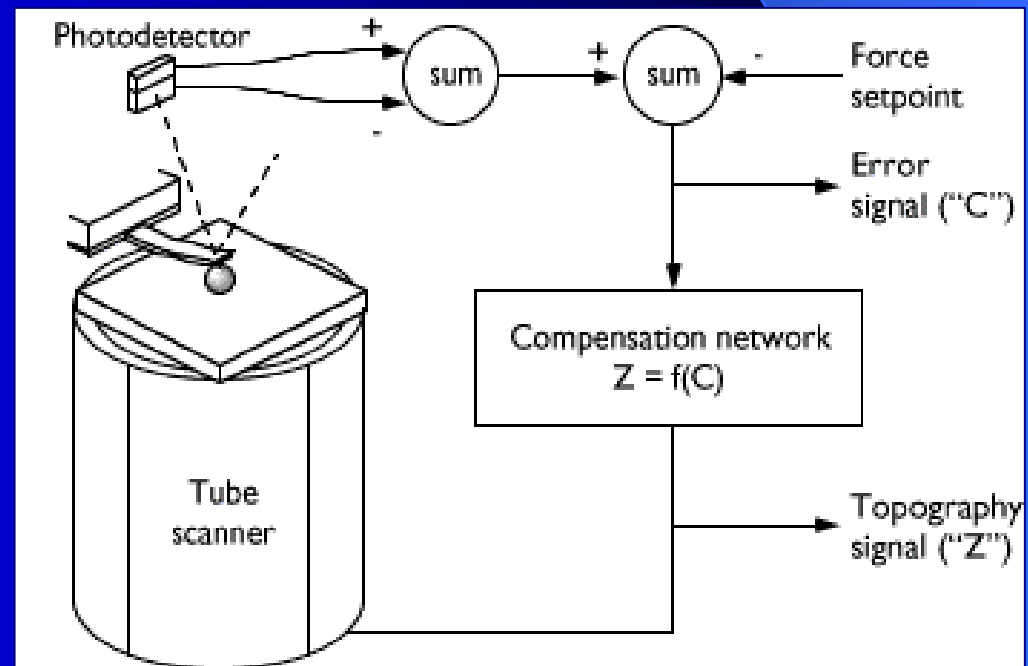
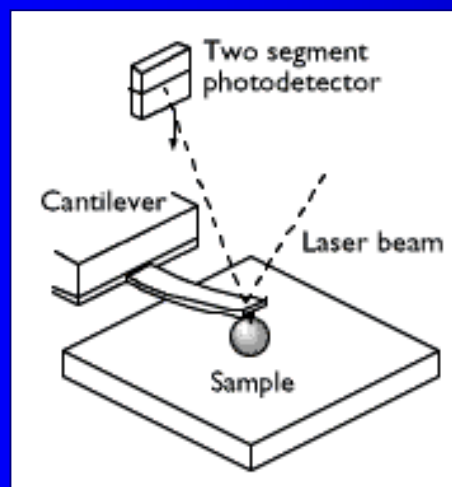
Hot-Film

Hot-wire at  $y/\delta = 0.1$



# AFM Surface Roughness Measurements

- Atomic Force Microscopy (AFM) was utilised to determine surface finish on the Nickel sensor.
- Apparatus consists of an atomically sharp silicon tip ( $3\ \mu\text{m}$  length) attached to the underside of a reflective micro-cantilever.
- Micro-stylus is moved back and forth over the material surface, the cantilever deflection is determined by an interferometric technique.

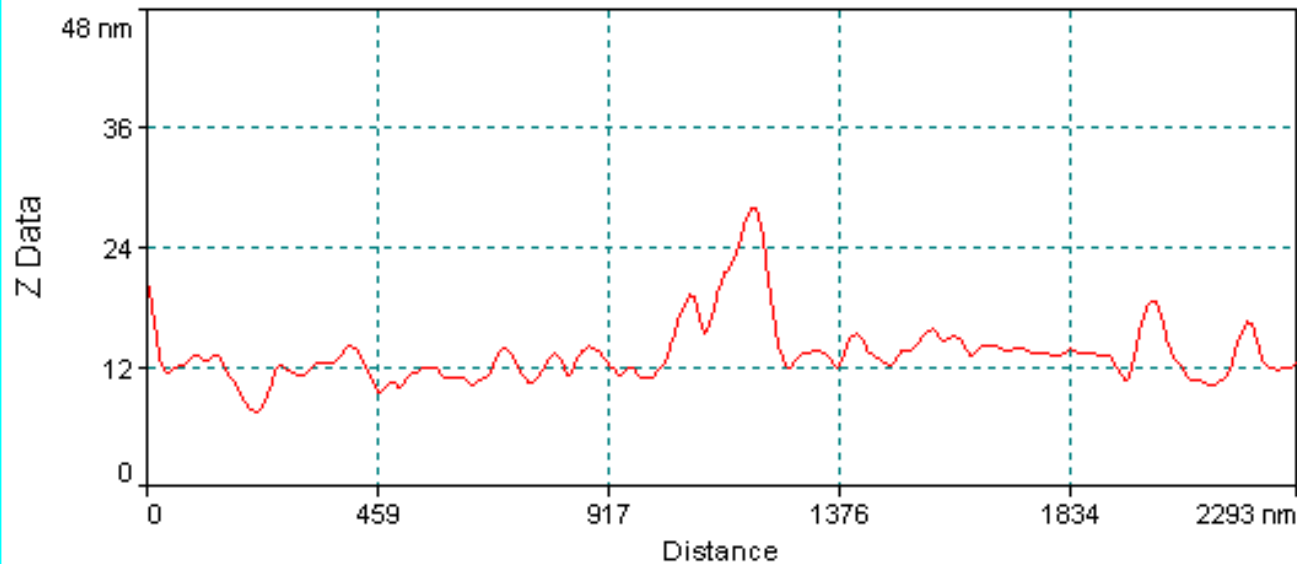
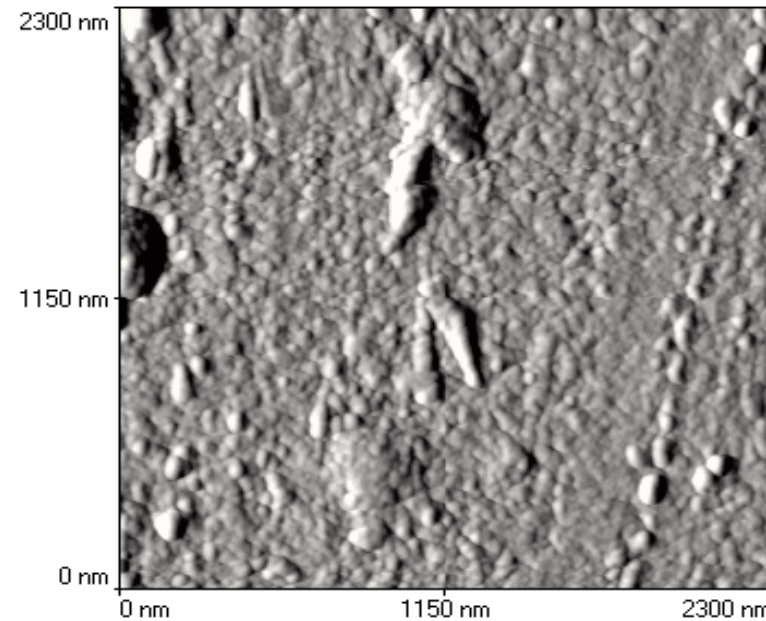


# AFM Surface Roughness Measurements

Whole Image

Area Ra: 3.4275 nm  
Area RMS: 5.0480 nm  
Avg. Height: 13.3402 nm  
Max. Range: 47.3579 nm

Ni Sensor Surface



## Conclusions

- **Hot-film and hot wire measurements correlate in close proximity to the wall.**
- **The strength of the correlation in the near-wall region is verified by the similarity between the wavelet transforms of a film and nearby hot-wire**
- **AFM measurements of surface roughness for the hot-film sensor are of the order of 20 nm, 100 times greater than molecular size.**