Graphene saturable absorbers for VECSELs

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ABSTRACT

We report mode-locking of an optically pumped VECSEL using a graphene-based saturable absorber mirror (GSAM). Self-starting and stable modelocked operation is demonstrated with 473 fs pulses at 1.5 GHz repetition rate and 949 nm center wavelength. Wavelength tuning is achieved over a 46 nm bandwidth. We discuss the mirror design, the fabrication of the GSAMs, and give an outlook on further optimization of the design, including dielectric top coatings to protect the graphene and to increase the flexibility in the design.

Keywords: VECSEL, graphene, mode-locking, broadband saturable absorber

1. INTRODUCTION

Ultrafast vertical-external-cavity surface-emitting lasers (VECSELs),^{1, 2} are excellent pulsed sources for various applications, such as multi-photon microscopy,³ optical data communications,² supercontinuum generation⁴ and ultracompact stabilized frequency combs.¹ VECSELs combine the advantages of semiconductor lasers, such as compactness,⁵ with those of diode pumped solid-state lasers, such as low timing jitter⁶, excellent beam quality,⁷ high average^{7, 8} and peak power^{4, 9}. The conventional devices used for modelocking of VECSELs are semiconductor saturable absorber mirrors (SESAMs)¹⁰ since they offer advantages such as an excellent ratio of saturable to non-saturable losses (e.g. 50:1¹¹) and a high damage threshold (>0.21 J/cm²)¹¹. However, SESAMs, epitaxially grown on lattice-matched semiconductor substrates¹⁰, only offer a limited operation bandwidth (to date, the broadest tuning range of VECSELs mode-locked with SESAMs is 13.7 nm)¹² and have a recovery time ranging from several hundreds of fs¹³ to tens of ps.¹¹ Graphene based saturable absorbers (GSAs) have emerged as a promising SAs for ultrafast pulse generation, since graphene offers broadband operation and ultrafast recombination dynamics in the order of tens of fs.^{14, 15} High quality, single layer graphene (SLG) can be grown¹⁶ and integrated in a variety of lasers.¹⁷ In common linear cavities, SLG is used as SA in transmission^{18, 19} resulting in a double-pass). While this allows to use GSA to modelock fiber^{16, 20, 21}, solid-state^{17, 19} and waveguid²² lasers, it poses limitations for VECSELs¹. These typically require a SA with losses <3% per cavity round-trip.^{23,24} Therefore, inserting a GSA in transmission (e.g. SLG on a quartz substrate¹⁹) inhibits lasing. To achieve self-starting passive modelocking of a VECSEL using a GSA it is crucial to reduce the total cavity roundtrip losses to <3% while maintaining a modulation depth in the range 0.5-2%.² We achieved this in Ref. 24 by controlling th

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2. MIRROR DESIGN

The structure consists of a highly reflecting mirror with a spacer and SLG on top. The thickness of the spacer changes the field intensity enhancement at the SLG and thus determines the absorption of the device.²⁴ The field intensity enhancement for a design wavelength λ in function of the thickness of the spacer layer *d* is then²⁴:

$$\xi_{\rm abs}(d) \approx \frac{4}{1 + n^2 \cot^2\left(\frac{2\pi}{\lambda} n \ d\right)},\tag{1}$$

where *n* is the refractive index of the spacer layer material. Using SiO₂ as spacer with thickness 0, $\lambda/12$ SiO₂, $\lambda/8$ SiO₂ and $\lambda/4$ SiO₂, the field intensity enhancement at the location of SLG ξ_{abs} is 0, 0.5, 1.3 and 4 (Figure 1 and Eq. 1). The absorption is²⁴ $A = \xi_{abs} \cdot 2.3\%$, where 2.3% is the absorption for SLG in transmission (corresponding to $\xi_{abs}=1$).



Figure 1. Spacer layer thickness dependent field intensity enhancement at the SLG location ξ_{abs} (left axis) and corresponding linear absorption (right axis), calculated (black line) compared to the absorption measurements (dots). Insets: Schematic view of four structures showing the last DBR mirror pairs with a) no SiO₂, b) $\lambda/12$ SiO₂ (55 nm), c) $\lambda/8$ SiO₂ (83 nm) and d) $\lambda/4$ SiO₂ (165 nm). The dark gray curve shows the normalized standing wave electric field intensity (for the design wavelength $\lambda=960$ nm) as a function of vertical displacement from the mirror surface. SLG (red) is the top layer.

3. FABRICATION AND CHARACTERIZATION

Four GSAMs are fabricated with spacers between the mirror and SLG by coating the mirror with: 0, $\lambda/12 \text{ SiO}_2$, $\lambda/8 \text{ SiO}_2$ and $\lambda/4 \text{ SiO}_2$. The high-reflection mirrors are anti-resonant distributed Bragg reflectors (DBRs).^{25, 26} DBRs typically consist of a stack of multiple layers with alternating high and low refractive index^{25, 26}, each with an optical thickness of a quarter of the design wavelength. The partial reflections at the layer interfaces interfere constructively resulting in high reflection (~100%).^{25, 26} We use 30-pair anti-resonant AlAs/GaAs (81.1 nm/67.85 nm) DBRs, designed to have a node of the standing wave at the surface of the top layer (anti-resonance) and a reflectivity >99.997 % at 960 nm. The DBRs are grown on a 3 inch 600 µm thick GaAs by molecular beam epitaxy (MBE), then cleaved into square 1 cm² pieces. Subsequently, the SiO₂ layers are deposited by plasma enhanced chemical vapor deposition with thickness of 0 nm, 55 nm ($\lambda/12$), 83 nm ($\lambda/8$) and 165 nm ($\lambda/4$) on different DBR samples (Figure 1(a-d)).

The SLG is grown by chemical vapor deposition (CVD) as discussed in Ref. 24. Subsequently it is transferred onto the SiO₂-coated DBRs.²⁴ A picture of the $\lambda/8$ SiO₂ sample is in Figure 2(a). The linear unsaturated absorption of the four

samples is measured with a high-precision reflectivity setup²⁷ giving A=0.25% (no SiO₂), 1.6% (λ /12 SiO₂), 3.2% (λ /8 SiO₂) and 10% (λ /4 SiO₂) at 960 nm. In Figure 1 those measurements show good agreement with the calculated values based on Eq. 1. Figure 2(b) plots the field intensity enhancement calculated from Eq.1 as a function of wavelength. The GSAMs reflectivity as a function of input light fluence (J/cm²) is characterized using the setup described in Ref. 27. The measurement for the λ /4 SiO₂ device (the GSAM with $\zeta_{abs}=4$) reveals a saturation fluence $F_{sat}\sim100 \,\mu$ J/cm² (corresponding to a peak intensity Ipeak ~1.0 GW/cm²) and a modulation depth ~5%.²⁴ The F_{sat} of the λ /8 sample is estimated ~200 μ J/cm², higher than the λ /4 sample, because the smaller field intensity enhancement at the absorber makes the device saturate at a higher fluence.²⁴



Figure 2. a) $\lambda/8$ GSAM used for the modelocking experiments: SLG transferred onto the AlAs/GaAs DBR with a layer of 83 nm SiO₂. The SLG is seen as shaded area, since the 83 nm SiO₂ thickness gives a high optical contrast in the visible range²⁸. b) Field intensity enhancement at the absorber vs. wavelength.



4. MODELOCKING AND WAVELENGTH TUNING

Figure 3. a) Sketch of the laser cavity, b) intensity autocorrelation trace and the fit to the auto correlation of a 473 fs sech² pulse, c) optical spectrum and d) Microwave spectrum of the repetition rate centered at 1.5 GHz and measured with a resolution bandwidth of 1 kHz.

To demonstrate the suitability for passive modelocking the $\lambda/8$ GSAM sample is used in a VECSEL cavity. The laser cavity setup is in Figure 3(a). The resonator mode and pump spot radius on the gain chip are 150 and ~30 µm on the absorber, using a concave folding mirror with 20 mm radius of curvature. With a quantum dot (QD) VECSEL gain chip we obtain stable modelocking with pulse duration of 473 fs, as shown in the autocorrelation trace in Figure 3(b). The spectrum is centered at ~950nm (Figure 3e) and the repetition rate is 1.5 GHz (consistent with the 10 cm cavity length). The average output power is 5 mW using an output coupling (OC) mirror with 0.1% transmission. The pulse fluence on the GSAM is~125 µJ/cm². The broad operation bandwidth is demonstrated using three VECSELs optimized for emission at 940, 950 and 970nm. An antireflection coated 20 µm thick fused silica etalon is used for wavelength tuning. The GSAM is not temperature controlled, and supports modelocking in a tuning range ~46 nm, from 935 to 981 nm.²⁴

5. PROSPECTIVE DESIGN OPTIMIZATION

The approach to optimize the spectral flatness of the device is to place the absorber in the antinode of the standing wave (in the field maximum) for the design wavelength. This is the case for the $\lambda/4$ GSAM (Figure 1d). But, this has $\xi_{abs}=4$, therefore too high absorption for VECSEL modelocking. By adding an additional dielectric layer on top of the SLG the field may be reduced, while keeping the SLG still in the anti-node. This is shown in Figure 4(b). Here a $\lambda/4$ SiO₂ (165 nm) layer between DBR and graphene places the absorber in the anti-node and a $\lambda/4$ Al₂O₃ (136 nm) layer reduces the field. Figure 4(b) shows the design of the $\lambda/8$ GSAM for comparison, with the same field intensity enhancement at the design wavelength of 960 nm.



Figure 4. a) Design with additional dielectric layer as top coating. Here the absorber is placed in the antinode and the field is reduced with the top coating to the field intensity enhancement of $\xi_{abs}=1.3$, b) design used for modelocking and the broadband tuning experiment with field intensity enhancement of 1.3 (at 960 nm) at the SLG absorber position.

In Figure 5 the field intensity enhancement is computed (using the transfer matrix algorithm for multilayer structures²⁹) in the wavelength range between 920 and 1000 nm. This shows an improvement in the wavelength independence of the field intensity enhancement, therefore absorption of the device, in comparison to the $\lambda/8$ GSAM. Furthermore this coating also acts as a protective top-coating.



Figure 5. Field intensity enhancement at the absorber vs. wavelength for the new design. The new design (dark blue) has a much weaker wavelength dependence compared to the $\lambda/8$ SiO₂ sample (light blue).

6. CONCLUSIONS

We reported on an approach to control the absorption of graphene on a mirror in the range between 0-10%. This enabled us to fabricate a GSAM for VECSEL modelocking with sub 500 fs pulses at 1.5 GHz pulse repetition rate. Wavelength tuning was achieved over a 46 nm bandwidth. We gave an outlook on further optimization of the design, including dielectric top coatings to protect the graphene and to further increase the spectral flatness.

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