

Low-Loss Integrated Nanophotonic Circuits with Layered Semiconductor Materials

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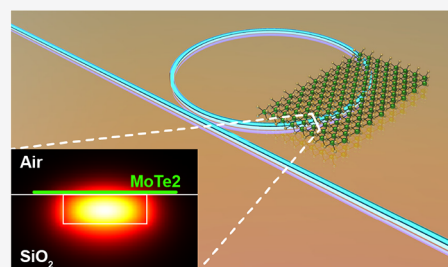
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ABSTRACT: Monolayer transition-metal dichalcogenides with direct bandgaps are emerging candidates for optoelectronic devices, such as photodetectors, light-emitting diodes, and electro-optic modulators. Here we report a low-loss integrated platform incorporating molybdenum ditelluride monolayers with silicon nitride photonic microresonators. We achieve microresonator quality factors $>3 \times 10^6$ in the telecommunication O- to E-bands. This paves the way for low-loss, hybrid photonic integrated circuits with layered semiconductors, not requiring heterogeneous wafer bonding.



KEYWORDS: photonic integrated circuits, silicon nitride, microresonators, layered materials, transition-metal dichalcogenides, MoTe₂

Layered materials (LMs),¹ such as graphene, transition-metal dichalcogenides (TMDs), and black phosphorus, are emerging platforms for applications in microelectronics,^{2–4} nanophotonics,^{5–8} and optoelectronics.^{9–12} Particularly important for optoelectronics are LMs with direct bandgaps, such as monolayer (1L) TMDs, enabling new physics and applications such as valleytronics,¹³ spintronics,¹⁴ transistors,¹⁵ light-emitting diodes (LEDs),¹⁶ modulators,¹⁰ and photodetectors.¹¹ Semiconducting TMDs undergo an indirect-to-direct bandgap transition when exfoliated from bulk to 1L,^{17,18} and their optical properties are dominated by excitonic transitions,^{19–21} typically in the visible or near-infrared ranges. E.g., 1L molybdenum diselenide (1L-MoSe₂) has a bandgap ~ 1.7 eV²² (~ 730 nm), and for 1L molybdenum ditelluride (1L-MoTe₂) this is ~ 1.1 eV^{23,24} (~ 1130 nm).

Strong light–matter interaction with LMs is beneficial for optoelectronics applications. One approach to enhance it is to integrate LMs with low-loss photonic microresonators.^{25–29} E.g., photodetectors employ resonant structures to significantly enhance the photon absorption and responsivity.³⁰ The performance of a microresonator depends not only on the mode volume, but also on the quality factor, defined as $Q = \omega/\kappa$, where $\omega/2\pi$ is the frequency of the optical mode and $\kappa/2\pi$ is the resonance line width.³¹ Q is a dimensionless parameter describing the energy stored in the microresonator divided by the energy dissipation per round trip.³¹ Thus, Q represents the power storing capability of a microresonator (i.e., the intracavity power enhancement with respect to the external optical field). In addition, Q is related to the intrinsic quality factor Q_0 (determined by light absorption and

scattering within the microresonator³²) and the external coupling Q_{ex} (determined by how strong the microresonator is coupled to the external optical field³³), as $Q^{-1} = Q_0^{-1} + Q_{ex}^{-1}$.

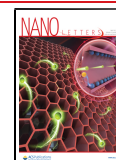
Planar photonic integrated circuits (PICs) are ideal platforms to enhance light–matter interactions with 1L-TMDs and to build new classes of high-performance integrated devices, such as LEDs, modulators, and photodetectors. The planarized top surfaces of waveguides and microresonators are advantageous, as the 1L-TMDs' flatness is maintained and strain-induced local fluctuations in the 1L-TMDs' band structure³⁴ are avoided. With deterministic transfer of 1L-TMDs,³⁵ these devices could be fabricated using CMOS technology with high yields⁷ and large volumes.³⁶ For most 1L-TMDs, their bandgaps for excitonic transitions lie in the visible range, while silicon (Si), commonly used in integrated photonics, has a transparency window³⁷ > 1.2 μm . This makes Si-based devices challenging for applications using TMDs, such as visible LEDs.

Silicon nitride (Si₃N₄)^{38,39} is a promising alternative to Si. It has a bandgap ~ 5 eV,⁴⁰ enabling a transparency window covering 400–2500 nm, free from two-photon absorption in the telecommunication bands. Refs. 41–45 reported inte-

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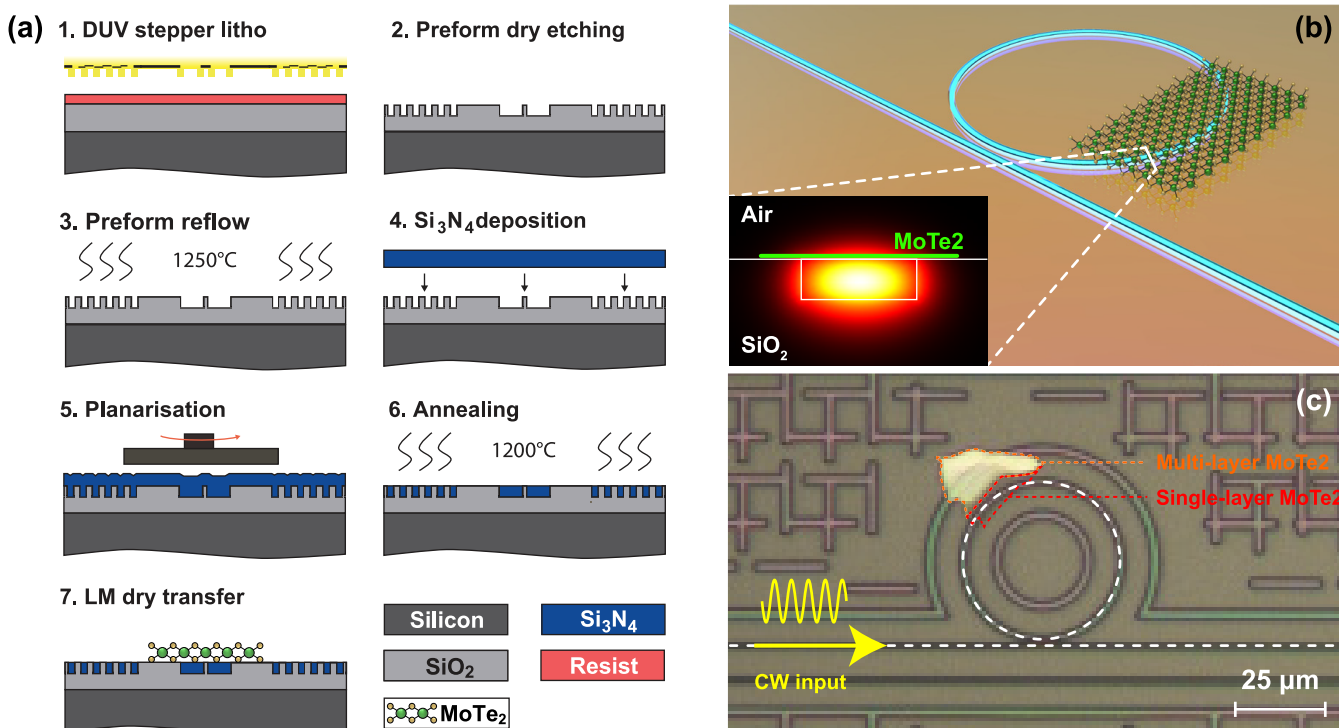


Figure 1. Fabrication process flow and sample overview. (a) Photonic Damascene reflow process to fabricate air-cladded, high-Q, Si_3N_4 microresonators and integration of 1L-MoTe₂. 1. Deep-UV stepper lithography is used to pattern the Si_3N_4 structures. 2. The pattern is transferred from the photoresist mask to the SiO_2 substrate via dry etching. 3. A preform reflow at 1250 °C reduces the waveguide sidewall roughness. 4. LPCVD Si_3N_4 is deposited on the patterned substrate, filling the trenches and forming the Si_3N_4 structures. 5. The excess Si_3N_4 is removed by CMP, ensuring a flat top surface. 6. The substrate is annealed at 1200 °C to drive out the residual hydrogen content in Si_3N_4 . 7. Dry transfer of LMs onto the Si_3N_4 microresonator. (b) Schematic of Si_3N_4 microring resonator covered with 1L-MoTe₂. (c) Optical microscope image showing Si_3N_4 microring resonator, bus waveguide, and MoTe₂. The white dashed line marks the Si_3N_4 ring resonator and bus waveguide, where light propagates.

grated Si_3N_4 waveguides with tight optical confinement and low losses ~ 1 dB/m, enabling microresonators with $Q^{42,45} > 30 \times 10^6$ and 1 m-long spiral waveguides in 20 mm² footprints.⁴⁵ In comparison, the lowest optical losses are still > 35 dB/m for both Si⁴⁶ and indium phosphide (InP)⁴⁷ because of the fabrication processes and the high refractive indices ($n_{\text{Si}} = 3.5$ and $n_{\text{InP}} = 3.2$ measured at the telecommunication bands) that enhance light scattering at the waveguide surface. Si_3N_4 has an excellent handling capability for high optical power > 100 kW.⁴⁸ Combining the high nonlinear index $n_2 = 2.5 \times 10^{-15}$ cm²W⁻¹ (describing the refractive index change induced by the optical intensity)³⁸ and the established geometry dispersion engineering (i.e., tailoring the group-velocity dispersion via geometry variation⁴⁹), Si_3N_4 has been used for various linear and nonlinear photonics applications based on light-matter interactions, particularly for microresonator-based Kerr frequency combs⁵⁰ and chip-based supercontinuum generation.⁵¹ Low-loss Si_3N_4 PICs are promising to study light-matter interactions with TMDs^{52,53} and have already been used to build modulators²⁹ and photodetectors.^{54,55} These active devices are also important for Si_3N_4 photonics, as Si_3N_4 is insulating and passive.

Here, we integrate Si_3N_4 microresonators with 1L-MoTe₂ and investigate the optical response of this Si_3N_4 -TMD hybrid system. 1L-MoTe₂ has a bandgap ~ 1.1 eV (~ 1130 nm^{23,24}). Thus, it is essentially transparent in the telecommunication bands 1280 - 1630 nm. We use photonic chip-based Si_3N_4 microring resonators with free spectral ranges (FSR, i.e. the frequency spacing of the optical resonance grid) of 150 GHz

and 1 THz. The $\text{FSR} = D_1/2\pi$, is calculated from the resonant condition $D_1/2\pi = c/(2\pi R \cdot n_g)$,⁵⁶ where c is the speed of light in vacuum and n_g is the group index of the optical mode (c/n_g being the group velocity of light). The Si_3N_4 microresonators, fabricated using the photonic Damascene process,⁵⁷ have no top SiO_2 cladding, thus the 1L-MoTe₂ transferred onto the Si_3N_4 waveguide's top surface can directly interact with the optical mode in the waveguide core.

Figure 1a presents the fabrication process flow for our Si_3N_4 PICs with LMs. The Si_3N_4 PIC is fabricated using the photonic Damascene process.⁵⁷ Deep-UV stepper lithography based on KrF at 248 nm is used to pattern Si_3N_4 waveguides, microresonators, and stress-release structures⁵⁷ (to prevent crack formation in Si_3N_4 due to the tensile film stress). The pattern is transferred from the photoresist mask to the SiO_2 substrate using dry etching based on C_4F_8 , O_2 , and He, followed by a preform reflow⁵⁸ at 1250 °C to reduce the waveguide surface roughness. Low-pressure chemical vapor deposition (LPCVD) based on SiH_2Cl_2 and NH_3 is used to deposit stoichiometric Si_3N_4 on the patterned preform, filling the trenches and forming the waveguide cores. The excess Si_3N_4 is removed by chemical-mechanical polishing (CMP), creating a flat top surface with a root-mean-square (RMS) roughness < 0.3 nm,⁵⁸ ideal to maintain the 1L-TMDs' flatness. The substrate is then annealed at 1200 °C to drive out the residual hydrogen introduced during LPCVD. There is a height difference < 40 nm between the Si_3N_4 waveguide cores and the surrounding SiO_2 cladding, as measured by scanning electron microscopy (SEM) and atomic force

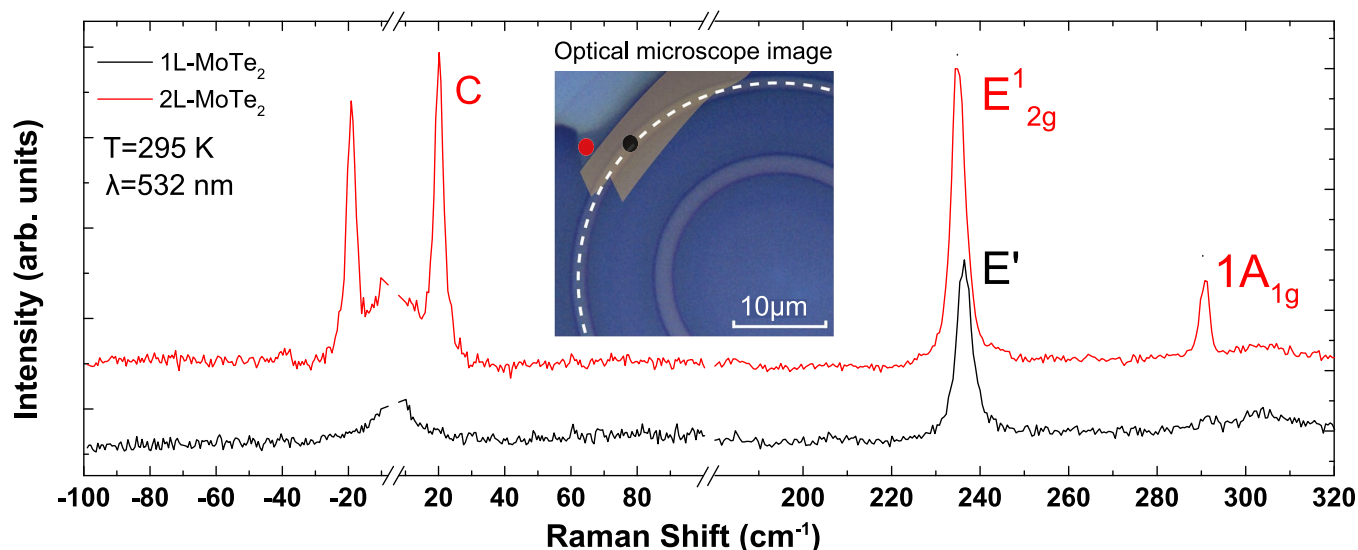


Figure 2. Raman spectra of 1L-MoTe₂ (black) on microresonator and 2L-MoTe₂ (red) outside it. Inset: optical microscope image of 1L-MoTe₂ on a Si₃N₄ microresonator. The black and red spots indicate where the representative Raman spectra of 1L- and 2L-MoTe₂ were measured. The white dashed line marks the Si₃N₄ microresonator, and the gray area is the 1L-MoTe₂ flake.

microscopy (AFM). This is caused by the post-CMP cleaning using buffered HF to remove the CMP slurry particles, and can be reduced by optimizing the cleaning process. The Si₃N₄ waveguides without top SiO₂ cladding allow seamless contact of 1L-MoTe₂ with the optical mode via evanescent coupling. This feature is a key advantage of the photonic Damascene process because of its additive fabrication nature. In comparison, the top-down, subtractive process^{59,60} requires complex control of the planarization, in order to create a flat wafer surface with bare waveguides.

1L-MoTe₂ flakes are exfoliated from bulk 2H-MoTe₂ crystals (alpha phase) prepared by flux zone growth⁶¹ on Nitto Denko tape¹⁷ and then exfoliated again on a polydimethylsiloxane (PDMS) stamp placed on a glass slide for inspection under an optical microscope. Optical contrast is used to identify 1L-MoTe₂ prior to transfer.⁶² Before 1L-MoTe₂ transfer, the Si₃N₄ microresonators are wet-cleaned by 60 s ultrasonication in acetone and isopropanol and exposed to oxygen-assisted plasma at 10 W for 60 s. The 1L-MoTe₂ flakes are aligned and stamped on the Si₃N₄ microresonators with a micromanipulator at 40 °C, before increasing the temperature to 60 °C, so the flakes detach from the PDMS and adhere preferentially to the microresonators.⁶³ Figure 1b illustrates a Si₃N₄ microring resonator covered with 1L-MoTe₂. Figure 1c shows the optical microscope image of the sample, with the white dashed line marking the Si₃N₄ bus waveguide and the microring resonator. Light is coupled from the bus waveguide to the microring resonator via in-plane evanescent coupling with a gap distance of 775 nm.

To characterize the transferred 1L-MoTe₂, we use micro-Raman spectroscopy at 532 nm (~2.3 eV), close to the C-exciton energy of MoTe₂,⁶⁴ to enhance the electron–phonon interaction^{65,66} in the vicinity of the Γ -point of the Brillouin zone. We use <50 μ W power to avoid thermal effects. The measurements are performed in a Horiba LabRam Evolution with a cutoff frequency ~5 cm⁻¹, a 1800 l/mm grating and a spot size ~700 nm. We measure 1L-MoTe₂ located on the microresonator (black dot in the inset of Figure 2), and compare it with a 2L-MoTe₂ flake out of the microresonator (red dot in the inset of Figure 2). The Raman spectra of 1L-

and 2L-MoTe₂ are also shown in Figure 2. A strong C mode^{67,68} is observed ~19.5 cm⁻¹ in 2L-MoTe₂ but is absent for 1L-MoTe₂, as expected.⁶⁹ The in-plane modes are ~236.4 cm⁻¹ for 1L-MoTe₂ (E' mode) and ~234.9 cm⁻¹ for 2L-MoTe₂ (E'₁₂g mode), in good agreement with literature.⁷⁰ The out-of-plane metal-chalcogen vibration (B_{2g} in bulk and 1A_{1g} in 2L-MoTe₂⁷⁰) is only observed in 2L-MoTe₂ ~290.8 cm⁻¹, because B_{2g} symmetry modes are inactive for 1L-MoTe₂.⁷⁰ This confirms the transfer of 1L-MoTe₂ on the microresonator.

To investigate the effect of the transferred 1L-MoTe₂ on the Si₃N₄ optical mode, we characterize the optical resonances of the integrated hybrid microresonator system. For integrated photonics, a comprehensive characterization of the optical properties of any passive devices often includes the real and imaginary parts of the effective refractive index, n_{eff} and k_{eff} (thus the full effective refractive index is $n_{\text{eff}} + ik_{\text{eff}}$).²⁹ For microresonators, n_{eff} and k_{eff} can be obtained from measuring the frequencies $\omega/2\pi$ and line widths $\kappa_0/2\pi$ of the resonance grid.³² These parameters are related via $Q_0 = \omega/\kappa_0 = n_{\text{eff}}/(2k_{\text{eff}})$. While the excitonic absorption of 1L-MoTe₂ in the telecommunication bands should be negligible, an increase of k_{eff} is expected as a result of transfer-induced extra optical loss. This is due to the imperfect transfer of 1L-MoTe₂ that can cause contamination or surface damage. Thus, the change of k_{eff} (i.e., Δk_{eff}) can be determined by measuring the line width increase or Q factor decrease before and after TMD transfer. Figure 3a shows our optical characterization setup. Light is coupled into and out of the Si₃N₄ chip using lensed fibers and double-inverse nanotapers at the chip facets.⁷¹ The total fiber-chip-through coupling efficiency, i.e. the ratio of the optical power in the output fiber to the power in the input fiber, is ~40%. To measure $\omega/2\pi$ and $\kappa_0/2\pi$, the optical transmission spectrum of the microresonator is calibrated using frequency-comb-assisted diode laser spectroscopy.^{72,73} Three mode-hop-free, widely tunable, external-cavity diode lasers (ECDLs) are used and cascaded⁷³ to cover the telecommunication O- to E-band (1280–1630 nm). When scanning, the instantaneous laser frequency is acquired by beating the laser with a commercial, self-referenced, fiber-

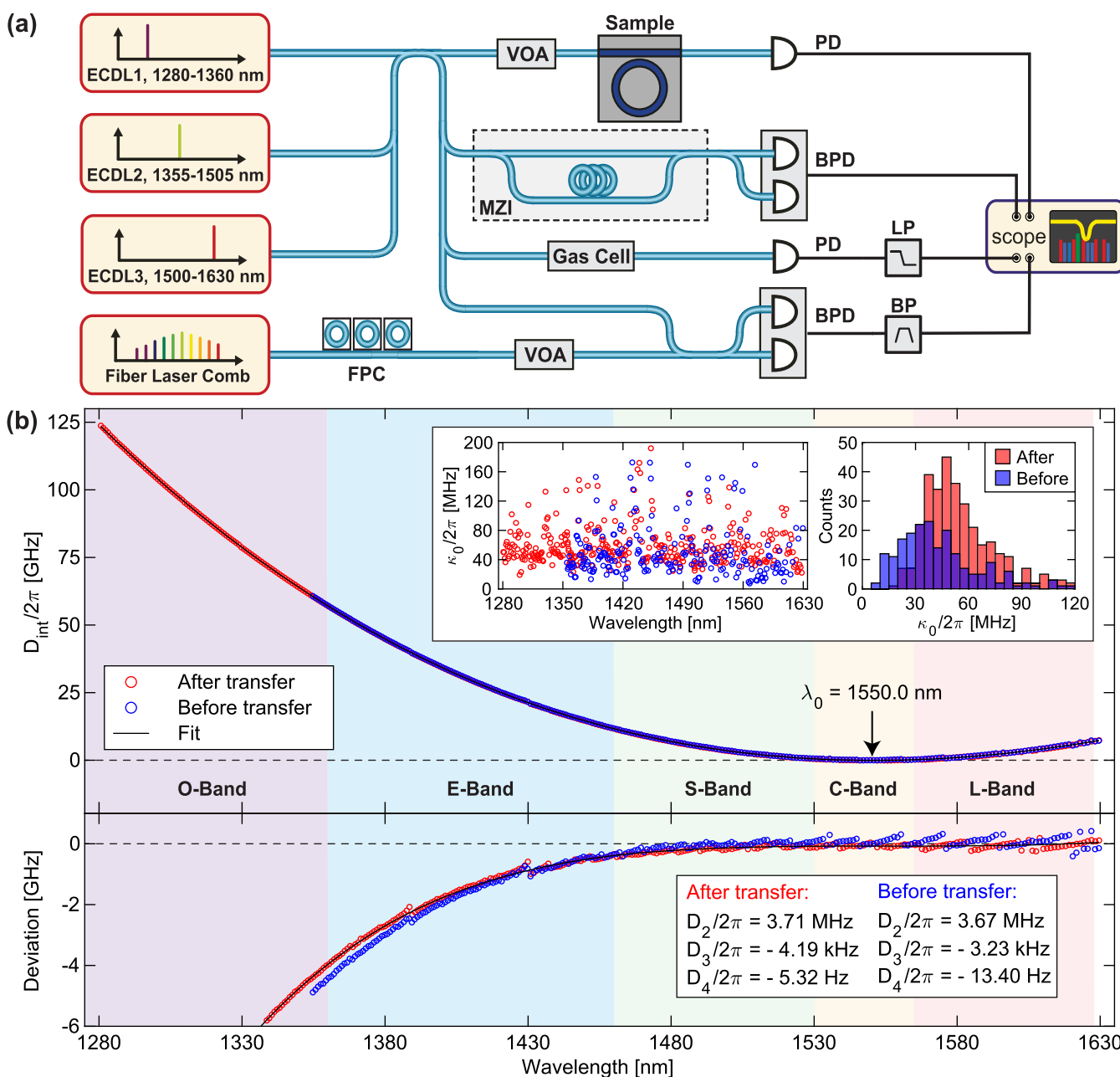


Figure 3. Experimental characterization of loss and dispersion of 150-GHz-FSR Si_3N_4 microresonator. (a) Frequency-comb-assisted cascaded diode laser spectroscopy used to characterize the microresonator. ECDL: external-cavity diode laser. FPC: fiber polarization controller. VOA: variable optical attenuator. MZI: Mach-Zehnder interferometer. PD(BPD): (balanced) photodetector. LP/BP: electronic low/band-pass filter. (b) Top: Measured integrated microresonator dispersion profile, $D_{\text{int}}/2\pi$, covering 1280 - 1630 nm for the TE_{00} mode. The reference resonance wavelength is 1550 nm. Insets: $\kappa_0/2\pi$ of each resonance, and $\kappa_0/2\pi$ histograms showing that the most probable value increases from 35 to 50 MHz after 1L-MoTe₂ transfer. Bottom: Resonance frequency deviation from the D_2 -dominant parabolic profile $[D_{\text{int}}(\mu) - D_2\mu^2/2]/2\pi$, to reveal the change in higher-order dispersion (such as $D_3/2\pi$) and avoided mode crossings.

laser-based optical frequency comb,⁷² assisted with a Mach-Zehnder interferometer.⁵⁷ Molecular absorption spectroscopy is also performed during the laser frequency scan,⁷³ to further calibrate the optical transmission spectrum of the microresonator, in order to extract the absolute frequency of each data point.

The light polarization is constant during the laser scan, as polarization-maintaining fiber components are used. Optical resonances in the microresonator transmission spectrum are identified and fitted,⁷⁴ to extract the microresonator's intrinsic loss $\kappa_0/2\pi$ and the bus-waveguide-to-microresonator external

coupling strength $\kappa_{\text{ex}}/2\pi$. The loaded line width is thus calculated as $\kappa/2\pi = \kappa_{\text{ex}}/2\pi + \kappa_0/2\pi$ (κ , κ_{ex} , and κ_0 are angular frequencies). Compared with previous studies on TMD-enabled PICs which analyzed the optical loss on a single wavelength⁵⁹ or a single resonance,⁶⁰ our optical characterization technique provides broadband wavelength-dependent information on $n_{\text{eff}}(\lambda)$ and $k_{\text{eff}}(\lambda)$, and can identify any absorption feature within the measurement band. Our transfer technique can thus be systematically optimized to achieve the lowest transfer-induced optical losses.

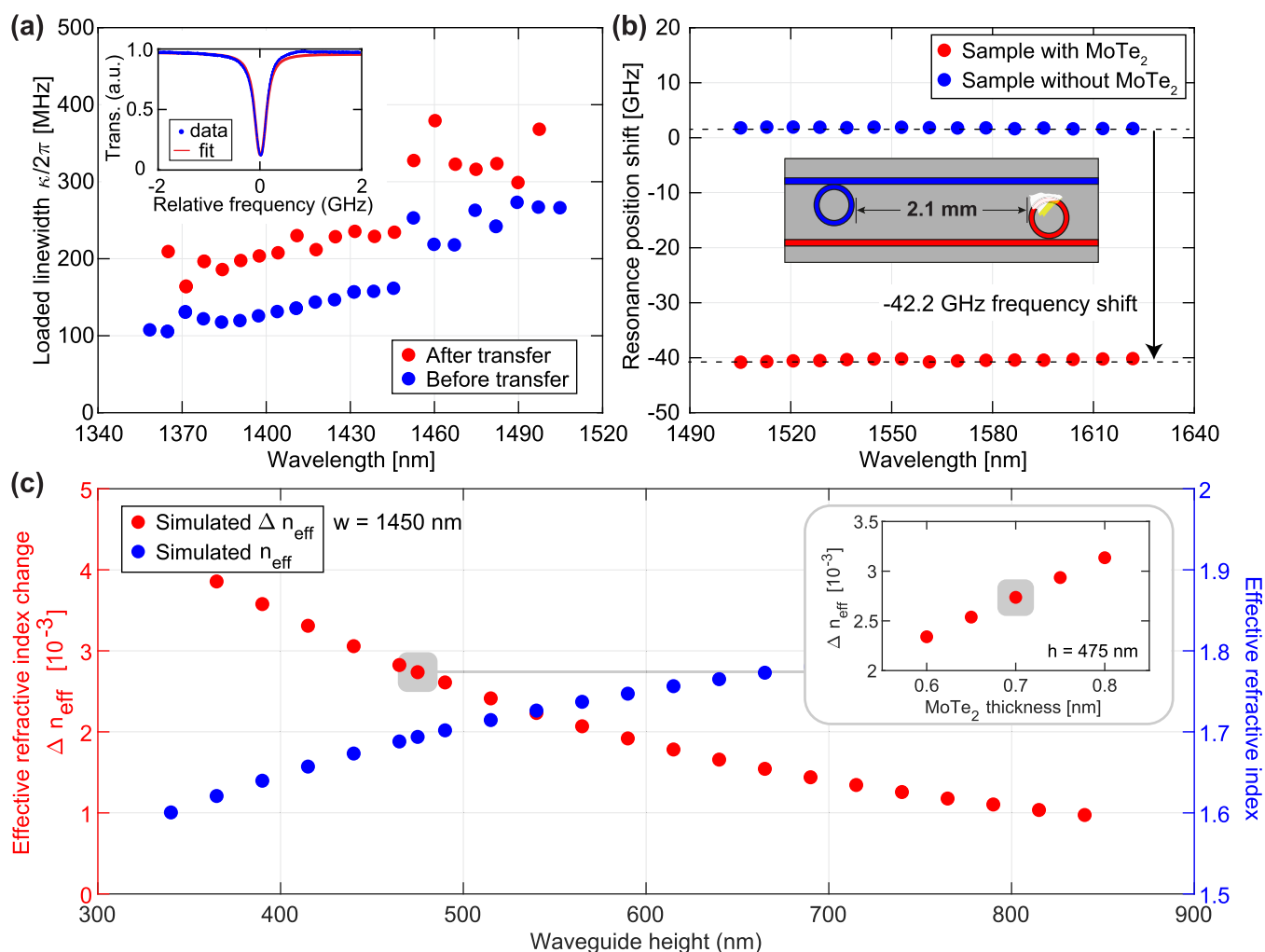


Figure 4. Experimental characterization and simulations of loss and resonance frequency shift of 1-THz-FSR Si_3N_4 microresonator with 1L-MoTe₂. (a) Measured $\kappa/2\pi$ before and after 1L-MoTe₂ transfer. Inset: representative resonance profile at 1425 nm and its Lorentzian fit, giving $\kappa_{\text{ex}}/2\pi = 82$ MHz and $\kappa_0/2\pi = 147$ MHz. (b) Measured and calculated absolute frequency shift of the TE₀₀ resonance grid before and after 1L-MoTe₂ transfer, for two microresonators, one with 1L-MoTe₂ and the other without. Inset: schematic showing that the two microresonators are 2.1 mm apart on the same chip. (c) Simulated n_{eff} and change Δn_{eff} of n_{eff} due to the presence of 1L-MoTe₂, as a function of Si_3N_4 waveguide height. The simulated wavelength is 1550 nm in the TE₀₀ mode in the 1-THz-FSR microresonator. Insets: simulated Δn_{eff} as a function of the MoTe₂ thickness.

1L-MoTe₂ flakes are transferred onto Si_3N_4 microresonators with two FSRs: 150 GHz and 1 THz. First, we characterize the 150-GHz-FSR microresonator. Here we mainly study the transverse-electric fundamental mode of the microresonator (TE₀₀ mode). We note that the transverse-magnetic fundamental mode (TM₀₀) has a higher loss than the TE₀₀ mode. We characterize the same Si_3N_4 microresonator before and after 1L-MoTe₂ transfer, for comparison and to extract any extra loss introduced by 1L-MoTe₂ transfer. The measured $\kappa_0/2\pi$ are plotted in the inset of Figure 3b. No wavelength-dependent $\kappa_0/2\pi$, before and after the transfer, is observed far above the 1L-MoTe₂'s excitonic resonance ~ 1130 nm.²³ Histograms of $\kappa_0/2\pi$ show that the most probable value increases from 35 to 50 MHz after transfer. This loss increment corresponds to a Q_0 degradation from 5.5×10^6 to 3.9×10^6 , representing a viable low-loss microresonator with TMD integration. To the best of our knowledge, this is the highest Q reported in LM-enabled PICs. Ref 75 pointed out that the transfer process can affect the transmission properties of a photonic device to such an

extent that no transmission can be measured. E.g. mechanical scratches or contaminations on the chip surface can be the loss sources.⁷⁶ Since our microresonator Q is high ($\sim 5.5 \times 10^6$, corresponding to 6 dB/m linear loss) and our loss characterization method is accurate, any loss increment down to the level of dB/m can be observed. This enables us to improve our LM transfer to minimize losses. The LM surface cleanliness is mostly associated with the speed and temperature used for transfer.^{77,78} With PDMS transfer, we were able to detect interlayer excitons in TMD-LM heterostructures (LMHs),⁷⁹ demonstrating that our process does not leave residues on the TMD surfaces, unlike ref 80. We also avoid any extra contact between the PDMS stamp and the PICs. The PDMS stamp is aligned using x , y , z and theta (i.e., relative angle between PDMS stamp and target substrate) motorized stages to the microring area, and only contacts the target area of the PIC surface. This minimizes the area of contact, avoiding additional contamination with undesired MoTe₂ flakes from the PDMS stamp on top of the waveguide, which would induce extra losses.

Since our characterization technique can measure all the resonance frequencies covering the O- to E-band, the dispersion properties of the integrated hybrid microresonator can be calculated as well. These are critical for target applications at required wavelengths. E.g., anomalous dispersion is necessary for Kerr nonlinear photonics.⁵⁰ The measured integrated microresonator dispersion, defined as^{72,81} $D_{\text{int}}(\mu) = \omega_{\mu} - \omega_0 - \mu D_1 = D_2\mu^2/2 + D_3\mu^3/6 + D_4\mu^4/24 + \dots$, is shown in Figure 3b, top. Here $\omega_{\mu}/2\pi$ is the frequency of the μ^{th} resonance, $D_1/2\pi$ is the microresonator FSR, $D_2/2\pi$ is the group-velocity dispersion, $D_3/2\pi$ and $D_4/2\pi$ are higher-order dispersion terms. The reference resonance frequency is $\omega_0/2\pi = 193.4$ THz (corresponding to $\lambda_0 = 1550$ nm). Limited by the size of the transferred flake, the D_{int} curves before and after transfer are nearly identical. To further investigate the dispersion change, the deviation from the D_2 -dominant parabolic profile, defined as $[D_{\text{int}}(\mu) - D_2\mu^2/2]/2\pi$, is shown in Figure 3b, bottom. Higher-order dispersion changes (e.g., $D_3/2\pi$ and $D_4/2\pi$) and avoided mode crossings⁸¹ are revealed. The measured parameters from fitting are $D_2/2\pi = 3.67$ MHz and $D_3/2\pi = -3.2$ kHz before 1L-MoTe₂ transfer, and $D_2/2\pi = 3.71$ MHz and $D_3/2\pi = -4.2$ kHz after transfer.

To confirm the coupling of the Si₃N₄ optical mode to 1L-MoTe₂, the same device is further characterized in the wavelength range 1050–1090 nm (near the 1L-MoTe₂ excitonic resonance ~ 1130 nm), using another ECDL operating in this wavelength range. A different microresonator with a gap distance ~ 370 nm between the bus waveguide and the microresonator is used, in which the small gap distance ensures sufficient evanescent coupling between bus waveguide and microresonator. Before 1L-MoTe₂ transfer, the mean loaded resonance line width is $\kappa/2\pi \sim 200$ MHz. After transfer, most of the resonances, previously visible, vanish. The remaining resonances detected have $\kappa/2\pi > 1$ GHz, corresponding to an average loss ~ 1.5 dB/cm near 1 μm wavelength. This value is averaged over the entire microresonator, despite the fact that only a small part of it is covered by 1L-MoTe₂. Comparing with the optical losses measured in the 1280–1630 nm range, this wavelength-dependent loss is consistent with the significant optical absorption $\sim 3.4\%$ at the 1L-MoTe₂ band edge²³ and confirms that 1L-MoTe₂ is coupled to the optical mode.

We then characterize the 1-THz-FSR microresonator with a ring radius of 22 μm . The smaller size leads to a large ratio of its perimeter covered by 1L-MoTe₂, $\eta \sim 13\%$. Figure 4a plots $\kappa/2\pi$ of the measured TE₀₀ resonances from 1355 to 1505 nm, before and after 1L-MoTe₂ transfer. The observed wavelength-dependence is due to the bus-waveguide-to-microresonator evanescent coupling (i.e., $\kappa_{\text{ex}}/2\pi$ is wavelength-dependent and is larger at longer wavelengths). For each resonance, due to 1L-MoTe₂ transfer, a line width increment $\Delta\kappa/2\pi$ of up to 80 MHz is observed. As 1L-MoTe₂ is thinner than 1 nm, and should not effect the evanescent coupling, we attribute this $\kappa/2\pi$ increment to the $\kappa_0/2\pi$ increment. Figure 4a inset shows a resonance at 1425 nm, after 1L-MoTe₂ transfer, where the Lorentzian fit gives $\kappa_{\text{ex}}/2\pi = 82$ MHz and $\kappa_0/2\pi = 147$ MHz, respectively. This indicates that 1L-MoTe₂ transfer introduces an extra loss. We estimate $Q_0 \approx 1.3 \times 10^6$, lower than the initial $Q_0 \approx 3.8 \times 10^6$. The average loss increment is ~ 0.15 dB/cm. Therefore, the estimated linear optical loss in the waveguide fully covered by 1L-MoTe₂ is $\alpha \approx 0.15 \times (13\%)^{-1}$ dB/cm = 1.2 dB/cm.

We also investigate the frequency shift of the resonance grid induced by 1L-MoTe₂. This provides information on the change of n_{eff} . Another identical microresonator is used as reference, on the same chip, 2.1 mm apart from that with 1L-MoTe₂. The absolute frequency of each TE₀₀ resonance is measured, before and after 1L-MoTe₂ transfer, for both microresonators. The relative frequency shift of each resonance, before and after transfer, is plotted in Figure 4b. The microresonator without 1L-MoTe₂ only has a small frequency shift ~ 1.8 GHz, likely due to environmental temperature change during measurement. The thermo-optic coefficient of Si₃N₄⁸² is $dn(\text{Si}_3\text{N}_4)/dT = 2.5 \times 10^{-5}/\text{K}$. Thus, the temperature-induced frequency shift coefficient is -2.4 GHz/K (negative sign indicates red shift). For the microresonator with 1L-MoTe₂, an average frequency shift of -40.4 GHz is observed. Including the 1.8 GHz frequency shift identified in the reference microresonator, the total frequency shift due to 1L-MoTe₂ is -42.2 GHz. Since a part of the light field is coupled into 1L-MoTe₂, this frequency shift is induced by the increment of n_{eff} .

Finite-element-method (FEM) simulations of the TE₀₀ mode using COMSOL Multiphysics are then performed to study n_{eff} and the resulting Δn_{eff} due to the presence of 1L-MoTe₂. Figure 4c plots the simulated n_{eff} and Δn_{eff} as a function of Si₃N₄ waveguide height at 1550 nm. Here the waveguide has a fixed width $w = 1.45$ μm and a varying height h from 340 to 840 nm. We include in the simulations the 40 nm height difference between Si₃N₄ waveguide core and SiO₂ cladding. Surface current density boundary conditions are used to model 1L-MoTe₂. We use $n(\text{MoTe}_2) = 4.43$,²³ with 0.7 nm layer thickness, close to the experimental value from AFM measurements^{5,23}.

The experimentally measured, average refractive index change is $\Delta n_{\text{eff, avg}} = n_{\text{eff}} \cdot \Delta f/f_0$, where f_0 is the resonance frequency and Δf is the frequency shift. Considering that the Si₃N₄ microresonator is not fully covered by 1L-MoTe₂, we can write $\Delta n_{\text{eff}} = \Delta n_{\text{eff, avg}}/\eta$, where $\eta = 13\%$ is the ratio of the microresonator perimeter covered by 1L-MoTe₂. Figure 4b gives $\Delta n_{\text{eff}} = 2.73 \times 10^{-3}$. This corresponds to the Si₃N₄ waveguide with $h = 475$ nm, with $\sim 0.3\%$ of the optical mode overlapping the 1L-MoTe₂. In comparison, the SEM-measured waveguide height from the sample cross-section is $h = 540$ nm, corresponding to $\Delta n_{\text{eff}} = 2.23 \times 10^{-3}$ in Figure 4c. Therefore, the experimental Δn_{eff} is close to the simulated one and further confirms the successful coupling between MoTe₂ and Si₃N₄.

In conclusion, we demonstrated the integration of 1L-MoTe₂ on Si₃N₄ photonic microresonators with $Q_0 = 1.3 \times 10^6$ for a 1-THz-FSR microresonator, and $Q_0 = 3.9 \times 10^6$ for a 150-GHz-FSR one, with an optical loss of 1.2 dB/cm in the waveguide fully covered by 1L-MoTe₂ in the telecommunication bands. Our Si₃N₄ photonic Damascene process is thus compatible with LM dry transfer. Wet transfer^{1,35} and CVD growth^{83–85} could also be used to integrate 1L-TMDs with larger surface areas. Combining this with low-loss Si₃N₄ spiral waveguides of extended lengths up to a meter,⁴⁵ high-responsivity, traveling-wave photodetectors could be built.⁸⁶ In addition, 1L-TMDs and single-layer graphene have a third-order-nonlinear susceptibility $\chi_3 \sim 10^{-18}$ m²/V² (refs 87,88) and $\chi_3 \sim 10^{-15}$ m²/V² (refs 89–91), significantly higher than that³⁸ of Si₃N₄ $\sim 10^{-21}$ m²/V². Therefore, LM-integrated, high-Q Si₃N₄ microresonators could be used to realize few-photon nonlinear optics, TMD-assisted four-wave mixing, and

cavity-enhanced frequency conversion.⁹² By maintaining the intrinsic low losses, our work paves the way to adding novel active functionalities on the Si₃N₄ photonics platform.⁹³

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Notes

The authors declare no competing financial interest.

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